4-19-09

# COVINGTON & BURLING LLP

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BEIJING BRUSSELS LONDON NEW YORK SAN DIEGO SAN FRANCISCO SILICON VALLEY WASHINGTON

August 18, 2009

#### BY FEDERAL EXPRESS

Federal Communications Commission Media Bureau P.O. Box 979089 St. Louis, MO 63197-9000

Attn: Video Division, Media Bureau

Re: KLOK(AM), San Jose, CA

Facility ID: 41339 FRN: 0004946141

# **Application for AM Broadcast Station**

Transmitted herewith, on behalf of Univision Radio License Corporation, the licensee of KLOK(AM), San Jose, California, are an original and three copies of the station's Application for AM Broadcast Station License on FCC Form 302-AM, together with an executed Form 159 Remittance Advice to cover the requisite filing fee. Also enclosed is an additional copy of the Application to be stamped as received and returned in the self-addressed pre-paid envelope provided.

Please direct any questions regarding this matter to the undersigned.

Respectfully submitted,

Mace J. Rosenstein

Counsel for Univision Radio License Corporation

Federal Communications Commission Washington, D. C. 20554

Approved by OMB 3060-0627 Expires 01/31/98

FOR FCC USE	
ONLY	

# FCC 302-AM APPLICATION FOR AM BROADCAST STATION LICENSE

(Please read instructions before filling out form.

FOR COMMISSION USE ONLY	. 1
FILE NO. BZ-20090819A	HK

			. /		
SECTION I - APPLICANT FEE INFORMATION					
PAYOR NAME (Last, First, Middle Initial)					
Covington & Burling LLP					
MAILING ADDRESS (Line 1) (Maximum 35 characters) 1201 Pennsylvania Avenue, NW					
MAILING ADDRESS (Line 2) (Maximum 35 characters)					
CITY Washington	STATE OR COUNTRY (if for DC	eign address)	ZIP CODE 20004		
TELEPHONE NUMBER (include area code) (202) 662-5023	CALL LETTERS KLOK	OTHER FCC IDE	NTIFIER (If applicable)		
2. A. Is a fee submitted with this application?	1		√ Yes No		
B. If No, indicate reason for fee exemption (see 47 C.F.R. Section		•			
Governmental Entity Noncommercial education	ational licensee Ot	her (Please explain	):		
C. If Yes, provide the following information:					
Enter in Column (A) the correct Fee Type Code for the service you a Fee Filing Guide." Column (B) lists the Fee Multiple applicable for this	are applying for. Fee Type Co	des may be found i	n the "Mass Media Services		
(a) which is a second of the control	application. Litter lee amoun	t due in Column (C	).		
(A)(B)	(C)				
FEE TYPE FEE MULTIPLE	FEE DUE FOR FEE TYPE CODE IN	1 1	FOR FCC USE ONLY		
M M R 0 0 1	\$ 615				
To be used only when you are requesting concurrent actions which resu	ult in a requirement to list more	than one Fac Turn	- Code		
(A) (B)	(C)	than one ree Type	s Code.		
M O R 0 0 1	<b>\$</b> 705		FOR FCC USE ONLY		
ADD ALL AMOUNTS SHOWN IN COLUMN C, AND ENTER THE TOTAL HERE.	TOTAL AMOUNT REMITTED WITH THIS APPLICATION	6	FOR FCC USE ONLY		
THIS AMOUNT SHOULD EQUAL YOUR ENCLOSED REMITTANCE.	\$ 1320				

SECTION II - APPLICANT INFORMATION					
1. NAME OF APPLICANT UNIVISION RAD	DIO LICENSE CORF	PORATI	ON		
MAILING ADDRESS 5999 CENTER DRI	VE	***************************************			
CITY Los Angeles			STATE CA		ZIP CODE 90045
2. This application is for:	Commercial	[	Noncomm	nercial	
	AM Dire	ctional	AM N	on-Directional	
Call letters	Community of License	Construct	ion Permit File No.	Modification of Construction	Expiration Date of Last
KLOK	San Jose	N/A		Permit File No(s). N/A	Construction Permit N/A
3. Is the station no accordance with 47 C.F.  If No, explain in an Exhil		to autor	matic program	test authority in	Yes No Exhibit No. N/A
4. Have all the terms construction permit beer If No, state exceptions in	•	ations se	et forth in the	above described	Yes No  Exhibit No. N/A
·					
<ol><li>Apart from the change the grant of the underly representation contained</li></ol>	ying construction permit	t which w	ould result in a	any statement or	Yes No
If Yes, explain in an Exh					Exhibit No.
6. Has the permittee file certification in accordance	ed its Ownership Report	(FCC For	m 323) or owne	rship	Yes No
continuation in accordance	se with 47 C.F.N. Section	173.3013	(b) r		✓ Does not apply
If No, explain in an Exhib	oit.				Exhibit No.
7. Has an adverse finding been made or an adverse final action been taken by any court or administrative body with respect to the applicant or parties to the application in a civil or criminal proceeding, brought under the provisions of any law relating to the following: any felony; mass media related antitrust or unfair competition; fraudulent statements to another governmental unit; or discrimination?					
If the answer is Yes, attach as an Exhibit a full disclosure of the persons and matters involved, including an identification of the court or administrative body and the proceeding (by dates and file numbers), and the disposition of the litigation. Where the requisite information has been earlier disclosed in connection with another application or as required by 47 U.S.C. Section 1.65(c), the applicant need only provide: (i) an identification of that previous submission by reference to the file number in the case of an application, the call letters of the station regarding which the application or Section 1.65 information was filed, and the date of filing; and (ii) the disposition of the previously reported matter.					

8. Does the applicant, or any party to the application, have a petition on file to migrate to the expanded band (1605-1705 kHz) or a permit or license either in the existing band or expanded band that is held in combination (pursuant to the 5 year holding period allowed) with the AM facility proposed to be modified herein?					
If Yes, provide particulars as an Exhibit.	Exhibit No.				
The APPLICANT hereby waives any claim to the use of any particular frequency or of the electromagnetic spectrum as against the regulatory power of the United States because use of the same, whether by license or otherwise, and requests and authorization in accordance with this application. (See Section 304 of the Communications Act of 1934, as amended).					
The APPLICANT acknowledges that all the statements material representations and that all the exhibits are a material	de in this application and attached exhibits are considered al part hereof and are incorporated herein as set out in full in				
CERTIFI	CATION				
1. By checking Yes, the applicant certifies, that, in the case of an individual applicant, he or she is not subject to a denial of federal benefits that includes FCC benefits pursuant to Section 5301 of the Anti-Drug Abuse Act of 1988, 21 U.S.C. Section 862, or, in the case of a non-individual applicant (e.g., corporation, partnership or other unincorporated association), no party to the application is subject to a denial of federal benefits that includes FCC benefits pursuant to that section. For the definition of a "party" for these purposes, see 47 C.F.R. Section 1.2002(b).					
Icer tify that the statements in this application are true, co and are made in good faith.	implete, and correct to the best of my knowledge and belief,				
Name Christopher G. Wood	Signature U V O S				
Title Vice President and Senior Legal Counsel	Date Telephone Number (310) 348-3600				
WILLELL FALSE STATEMENTS ON THIS EODS AD	E DUMOUL DU E DU EUR				

# (U.S. CODE, TITLE 18, SECTION 1001), AND/OR REVOCATION OF ANY STATION LICENSE OR CONSTRUCTION

FCC NOTICE TO INDIVIDUALS REQUIRED BY THE PRIVACY ACT AND THE PAPERWORK REDUCTION ACT

The solicitation of personal information requested in this application is authorized by the Communications Act of 1934, as amended. The Commission will use the information provided in this form to determine whether grant of the application is in the public interest. In reaching that determination, or for law enforcement purposes, it may become necessary to refer personal information contained in this form to another government agency. In addition, all information provided in this form will be available for public inspection. If information requested on the form is not provided, the application may be returned without action having been taken upon it or its processing may be delayed while a request is made to provide the missing information. Your response is required to obtain the requested authorization.

Public reporting burden for this collection of information is estimated to average 639 hours and 53 minutes per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing the burden, can be sent to the Federal Communications Commission, Records Management Branch, Paperwork Reduction Project (3060-0627), Washington, D. C. 20554. Do NOT send completed forms to this address.

THE FOREGOING NOTICE IS REQUIRED BY THE PRIVACY ACT OF 1974, P.L. 93-579, DECEMBER 31, 1974, 5 U.S.C. 552a(e)(3), AND THE PAPERWORK REDUCTION ACT OF 1980, P.L. 96-511, DECEMBER 11, 1980, 44 U.S.C. 3507.

Name of Applica		CATION ENGI	NEERING DATA				
, ,		Radio Licens	se Corporatio	n			
PURPOSE OF A	UTHORIZATIO	N APPLIED FOR	: (check one)				
<u>v</u>	Station License		Direct Mea	surement of Pov	ver		
1. Facilities auth							
Call Sign		struction Permit	Frequency	Hours of Oper	ation		kilowatts
KLOK	(if applicable)		(kHz) 1170	unlimit	ted	Night 5	<sup>Day</sup> 50
2. Station location	on			T			
State Ca	alifornia			City or Town	San Jose		
3. Transmitter lo	cation						
State	County			City or Town		Street address (or other identific	ation)
CA	San	ta Clara			San Jose	2905 S. Ki	
4. Main studio lo	cation			· ·		I	
State	County			City or Town		Street address (or other identific	ation)
CA	Sar	Francisco		San Fr	ancisco	` 750 Batter	
5. Remote contro	ol point location	(specify only if a	uthorized direction	ial antenna)			
State	County			City or Town		Street address (or other identific	ation)
6. Has type-approved stereo generating equipment been installed?  7. Does the sampling system meet the requirements of 47 C.F.R. Section 73.68?  Yes Vo  No  Not Applicable  Attach as an Exhibit a detailed description of the sampling system as installed.  Exhibit No.  "Engineering"							
8. Operating con		rent (in amperes	) without	RF common p	oint or antenna	current (in amper	es) without
modulation for nig		9.5	,	modulation for		29.6	
Measured antenna or common point resistance (in ohms) at operating frequency Night 60.0  Day 60.0  Measured antenna or common point reactance (in ohms) at operating frequency Night 0  Day 0							
Antenna indicatio	ns for direction						
Antenna monitor Antenna monitor sample Towers Phase reading(s) in degrees current ratio(s)  Antenna base curre			pase currents				
		Night	Day	Night	Day	Night	Day
2		-84.7° 0.0°	+146.2° -57.0°	0.485 1.000	0.633 0.674		
3		+88.1°	0.0°	0.570	1.000		
Manufacturer and	I type of antenna	a monitor:	1		1		

# SECTION III - Page 2

9. Description of antenna system ((f directional antenna is used, the information requested below should be given for each element of the array. Use separate sheets if necessary.)

	-					
Type Radiator Uniform cross-section Guyed	Overall height in meters of radiator above base insulator, or above base, if grounded.	Overall height above ground obstruction lig	(without	Overall height in met above ground (include obstruction lighting)	de   I	f antenna is either top oaded or sectionalized, describe fully in an Exhibit.
	66.9	68.6		69.2		
Excitation	Series	Shunt				
Geographic coordinates tower location.	to nearest second. For direct	tional antenna	give coordinate	es of center of array. F	For single	e vertical radiator give
North Latitude 37	° 18 '	41 "	West Longitu	<sup>de</sup> 121 <sup>o</sup>	48 '	58 "
	ove, attach as an Exhibit furth er and associated isolation ci		dimensions in	cluding any other	["	Exhibit No. Engineering"
Also, if necessary for a dimensions of ground sys	complete description, attac stem.	h as an Exhil	oit a sketch o	f the details and	"	Exhibit No. Engineering"
10. In what respect, if ar permit?  None	ny, does the apparatus consti	ructed differ fro	m that describ	ed in the application fo	or constru	uction permit or in the
11. Give reasons for the change in antenna or common point resistance.  Final adjustments resulted in slight changes from previous common point resistance.						
I certify that I represent information and that it is	the applicant in the capacity rue to the best of my knowled	indicated belo dge and belief.	w and that I h	ave examined the for	egoing s	tatement of technical
Name (Please Print or Ty Mark D. Neumar	, ,	S	ignature (chec	sk appropriate box beld	Neu	
Address (include ZIP Coo Hammett & Ediso	,		ate Au	igust 11, 2009		
Box 280068		Т	elephone No.	(Include Area Code)		
San Francisco, C	California 94128		707	7/996-5200		
Technical Director		V	Registered	d Professional Engine	er	
Chief Operator			Technical	Consultant		
Other (specify)						

FCC 302-AM (Page 5)

### Statement of Hammett & Edison, Inc., Consulting Engineers

The firm of Hammett & Edison, Inc., Consulting Engineers, has been retained by Univision Radio License Corporation, licensee of Radio Station KLOK, 1170 kHz, San Jose, California, to prepare the engineering portion of an application to relicense that station under the new method-of-moment technique allowed under FCC Rules Section 73.151(c).

#### Background

Radio Station KLOK, FCC Facility ID No. 41339, broadcasts at 50 kW day and 5 kW night, DA2, from an existing site in San Jose, California. The broadcast facility is located in a congested urban area where constant construction over the last 20 years has presented an ongoing problem with maintaining the KLOK monitoring points. As a result, the license has elected to take advantage of the most recent changes to FCC Rules Section 73.151(c), allowing use of moment method computer modeling to relicense the KLOK daytime and nighttime arrays. The KLOK tower base parameters have been determined to be in accordance with the requirements of that rule section and the phasing system has been adjusted to produce antenna monitor parameters within the required ±5 percent in ratio and ±3 degrees in phase of the modeled value. A summary of the KLOK site and facility information is given in Figures 1–3.

#### **Array Geometry**

The KLOK site layout is provided in Figure 2A. The final "as-built" tower positions are provided in the included Certified Survey (Figure 2B). The deviation in tower positions from their theoretical locations, when converted to electrical degrees at 1170 kHz, is less than 1° in relative position.

#### Impedance Measurements

Tower base impedance measurements were made by the undersigned at the final J-plugs within the antenna tuning units ("ATUs") using an Array Solutions PowerAim 120, S/N 1008, network analyzer. The other towers were all open circuited at the final J-plugs for each of the measurements.

#### **Method of Moments Model**

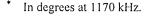
A method-of-moments model was created for each tower with the other towers opened at the base using Expert MININEC Broadcast Professional, Version 12.5. A -j10,000  $\Omega$  load was used for the assumed stray capacitance to ground. The method-of-moments model meets all FCC Rule requirements for model tower radius, height, and segment length, and calculation reference point, maximum hook-up inductance, and maximum shunt capacitance.

Tower	Physical Height*	Modeled Height*	Modeled Percentage	Modeled Radius	Circumference versus Total Face Width
1 2	94.0° 94.0°	100.0° 100.0°	106% 106%	0.29 m 0.44	100% 100%
3	94.0°	99.0°	105%	0.29	100%
Tower	Hook-up Inductance	Equival Induct		Z <sub>ATU</sub> Modeled	Z <sub>ATU</sub> Measured
1 2 3	30.9 Ω 28.4 23.4	3.7 µl 3.4 2.8	Н	59.8 + j100.6 Ω 59.0 + 96.1 57.5 + 88.4	$60.0 + 100.0 \Omega$ $59.4 + 96.0$ $57.2 + j88.7$

The modeled and measured base impedances at the ATU output jacks with the other towers open-circuited at their ATU output jacks agree within  $\pm 2$  ohms and  $\pm 4$  percent for resistance, as required by the FCC Rules. The MININEC Broadcast Pro model summaries for the three KLOK towers are provided in Figure 4.

#### **Derivation of Base Parameters**

The array of towers was modeled using Expert MININEC Broadcast Professional, Version 12.5. The wire end points were specified using polar coordinates with distances in electrical degrees at 1170 kHz. Each tower was modeled using 12 segments for individual segment lengths of 8.3°. The individual tower characteristics were adjusted, as noted above, to match the measured ATU output impedance. The permitted field parameters for the KLOK daytime and nighttime arrays were used with the "Medium Wave Array Synthesis" feature of MININEC to derive the driving point parameters at the ATU output where the current sampling transformers are installed.





#### **Daytime Base Parameters**

The MININEC Broadcast Pro model summary for the KLOK daytime array is provided in Figure 5. Absolute and relative tower base currents and phases are calculated to be:

Tower	Magnitude	Absolute Phase	Ratio	Relative Phase
1	12.60 A	+8.1°	0.633	+146.2°
2	13.41	+164.9°	0.674	-57.0°
3	19.91	+221.9°	1.000	$0.0^{\circ}$

#### **Daytime Antenna Monitor Parameters**

Based upon the results provided by MININEC, the array was adjusted and the antenna monitor parameters were set as follows:

Tower	Ratio	Phase
1	0.623	+146.2°
2	0.675	-57.2°
3	1.000	$0.0^{\circ}$

#### **Nighttime Base Parameters**

The MININEC Broadcast Pro model summary for the KLOK nighttime array is provided in Figure 6. Absolute and relative tower base currents and phases are calculated to be:

Tower	Magnitude	Absolute Phase	Ratio	Relative Phase
1	3.44 A	+282.8°	0.485	-84.7°
2	7.09	+7.5°	1.000	0.0°
3	4.04	+95.6°	0.570	+88.1°

#### **Nighttime Antenna Monitor Parameters**

Based upon the results provided by MININEC, the array was adjusted and the antenna monitor parameters were set as follows:

Tower	Ratio	<u>Phase</u>
1	0.488	-84.1°
2	1.000	$0.0^{\circ}$
3	0.560	+88.0°

Upon completion of the KLOK adjustments, the common point impedance for the KLOK daytime and nighttime arrays were measured by the undersigned using Array Solutions PowerAim 120, S/N 1008 network analyzer. Both common points were adjusted to  $60 + j0 \Omega$  and the common point currents were set to 29.6 A for the KLOK 50 kW daytime operations and 9.5 A for the KLOK 5 kW nighttime operation.



#### Sample System Proof

Impedance measurements were made of the antenna monitor sampling system by the undersigned, using an Array Solutions PowerAim 120, S/N 1008 network analyzer in a calibrated measurement system. The measurements were made into the antenna monitor ends of the sampling lines open-circuited to obtain line lengths and with the Delta TCT-1 current sampling transformers connected. In order to determine the characteristic impedance values of the sampling lines, open-circuit measurements were made with frequencies offset to produce  $\pm 45^{\circ}$  of electrical length from resonance frequency nearest to carrier (1016.9 kHz).

The sample lines meet all requirements of the FCC rules. They are within 1° of electrical length and the characteristic impedances are within 2 ohms of the nominal value. The sample line measurements made with the toroids connected are all within  $0.1 \Omega$  of each other.

The current sampling transformers were calibrated using the AM-19 antenna monitor. All three toroidal transformers were installed on a single bus and connected with equal length sample lines to the AM-19 antenna monitor. With one toroid set to reference (Ratio/Phase =  $1.000/0.0^{\circ}$ ), the antenna monitor readings for both of the other toroids were  $1.000/0.0^{\circ}$  and  $1.000/0.1^{\circ}$ , well within the manufacturer's specifications. Complete sample system proof results are provided in Figure 7.

### **Reference Field Strength Measurements**

Reference field strength measurements were made by the undersigned on July 31, 2009, using a Potomac Instruments Model FIM-41 field strength meter, S/N 319, on the azimuths for the four daytime and four nighttime radials specified in the KLOK license as monitor point radials. Point descriptions and field strengths are provided in Figure 8.

### Spurious Emissions Measurements

Emission measurements were made by the undersigned on May 21, 2009, using a Rohde & Schwarz spectrum analyzer, Model FSL6, S/N 100183, and a Potomac Instruments FIM 41 field strength meter, S/N 319, both under current calibration by the manufacturer. Measurements were made with KLOK operating at full power in daytime and nighttime modes. Specific results are given in Figure 9. No emissions were found in excess of those allowed by Section 73.44 of the FCC Rules.

#### Radio Frequency Exposure

No material changes were made to the KLOK licensed daytime or nighttime facilities other than minor changes in the antenna monitor parameters and the installation of new Delta Electronics Model TCT-1 current sampling transformers in the three ATUs. Therefore, no changes have been made in RF exposure conditions at the site with respect to presently licensed operation.

The entire KLOK site is fenced and the transmitter building is locked and accessible only to authorized personnel. The phasing cabinets are enclosed and interlocked so that access to the phasor is not available while the transmitter is in operation.

Based upon a maximum power in any of the KLOK towers of less than 25,000 watts, the distance to fields in excess of the FCC exposure limit applicable at 1170 kHz using the FCC Form 301 distance tables would be less than 13 feet for any tower.

The individual tower compounds are fenced out to a distance of 25 feet from each tower. The tower compound fences are six feet in height and have climbing deterrents installed. The compound gates are locked and appropriate warning signs are in place on the fences surrounding each tower compound.

Based on the information and analysis above, it is the undersigned's professional opinion that the KLOK broadcast site complies with the FCC guidelines limiting public exposure to radio frequency energy and, therefore, does not for this reason cause a significant impact on the environment.

#### Conclusion

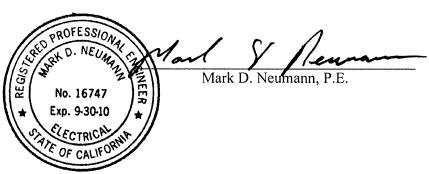
The KLOK array has been adjusted and is operating in accordance with the requirements set forth in Section 73.151 of the Commission Rules. A grant of license under the new method-of-moment rules is, therefore, requested.

#### **List of Figures**

In carrying out these engineering studies, the following attached figures were prepared under my direct supervision:

- 1. Engineering specifications of system as installed
- 2. Antenna system drawing
- 3. Circuit diagram
- 4. Tower method-of-moments model data
- 5. Daytime array method-of-moments model data
- 6. Nighttime array method-of-moments model data
- 7. Sample system proof
- 8. Reference point measurements
- 9. Harmonic and spurious measurements.

August 11, 2009



#### **Engineering Specifications As Installed**

#### A. Transmitter Site

Geographical Coordinates (NAD27)

37° 18' 41" N 121° 48' 58" W

2905 South King Road, San Jose, California

#### B. Studio & Remote Control Point

750 Battery Street, San Francisco, California

#### C. Equipment

Transmitter

Day, Nautel XL-60

50 kW

Night, Nautel ND-5

5 kW

Antenna monitor

Potomac, Model AM-19

#### D. Operation

Frequency

1170 kHz

Power

50 kW/5 kW

Hours of operation

Unlimited

Mode of operation

DA<sub>2</sub>

#### E. Antenna System

Number of towers

Three

Type of towers

Uniform cross-section, guyed

Height of towers above base insulator Overall height of towers above ground

Elevation of site above mean sea level

66.9 m 69.2 m\*

45.7 m

Overall height of towers above mean sea level

114.9 m\*

Field ratio and phase of towers

See Figure 2

Orientation of towers

See Figure 1B

Ground system

See Figure 2

Unlighted center tower is 68.6 m AGL and 114.3 m AMSL, respectively.



### **Engineering Specifications As Installed**

### **Daytime Theoretical Field Parameters**

	Tower 1	Tower 2	Tower 3
		(reference)	
Field ratio	1.000	1.000	1.300
Phase	0.0°	155.0°	-145.0°

#### Daytime Calculated Base Parameters†

	Tower 1	Tower 2	Tower 3
			(reference)
Field ratio	0.633	0.674	1.000
Phase	+146.2°	-57.0°	0.0°

### Daytime Antenna Monitor Parameters‡

	Tower 1	Tower 2	Tower 3
Field ratio	0.623	0.675	1.000
Phase	+146.2°	-57.2°	0.0°

Measured common point or base impedance	60 ohms
Common point or base current	29.6 A
Common point or input power	52.65 kW

<sup>&</sup>lt;sup>‡</sup> As adjusted.



<sup>&</sup>lt;sup>†</sup> Calculated Parameters have been referenced versus Tower 3 in order to make the maximum field ratio 1.000 for direct comparison with the Operating Parameters.

# **Engineering Specifications As Installed**

### **Nighttime Theoretical Field Parameters**

	Tower 1	Tower 2	Tower 3
Field ratio	1.000	1.920	1.000
Phase	-93.0°	0.0°	+93.0°

### Nighttime Calculated Base Parameters§

	Tower 1 Tower 2 Tower		
		(reference)	
Field ratio	0.485	1.000	0.570
Phase	-84.7°	0.0°	+88.1°

### Nighttime Antenna Monitor Parameters\*\*

	Tower 1	Tower 2	Tower 3
Field ratio	0.488	1.000	0.560
Phase	-84.1°	$0.0^{\circ}$	+88.0°

Measured common point or base impedance 60 ohms

Common point 9.5 A

Common point 9.5 A

Common point 5.4 kW

<sup>§</sup> Calculated Parameters have been referenced versus Tower 2 in order to make the maximum field ratio 1.000 for direct comparison with the Operating Parameters.





120 copper radials per tower, 64 m long or terminating at transverse copper strap or property boundary.

The number of radials for Tower 3 between approximately 350°T and 30°T is reduced due to the siting of a former studio building.

If m by 16 m copper mesh screens are installed at the base of each tower.

Uniform cross-section guyed towers.

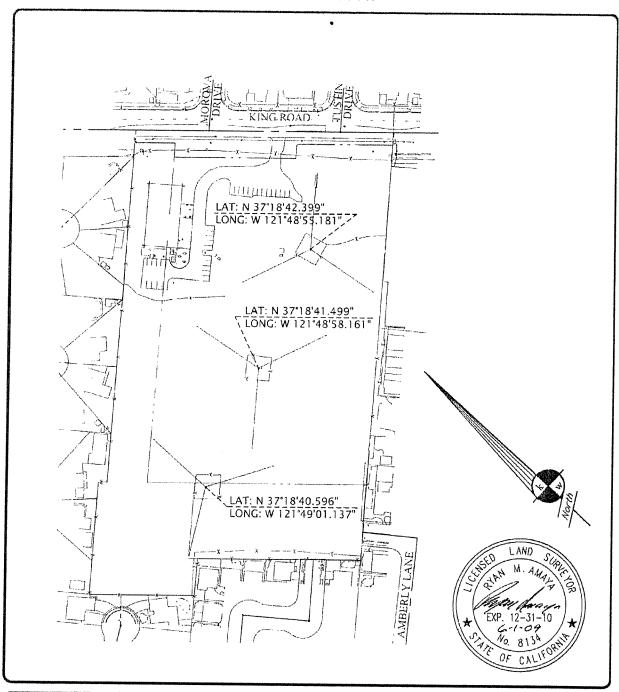
ASR Nos. 1250198, 1250199, and 1250171.

50 0 meters 50 100

		nitted Geometry	Survey From F	Results igure 2B	Deviati Specified	on from Location
Tower	Bearing	Distance	Bearing	Distance	Bearing	Distance
1	Ref.	Ref.	Ref.	Ref.	Ref.	Ref.
2	70.0°	110.0°	69.2°	110.1°	0.8°	0.1°
3	70.0°	220.0°	69.2°	220.0°	0.8°	$0.0^{\circ}$



Site Boundary



RADIO TOW	DATE	JUNE 2009	
FOR: UNIVIS	SCALE	1"=150'	
SAN JOSE	CALIFORNI	A DR. BY	SB
NAD 27 DATUM	KIER & WRIGHT	JOB	A03228-4
(LATITUDE & LONGITUDE)	CIVIL ENGINEERS & SURVEYORS, INC 3350 Scott Boulevard, Building 22 (408) 727 666		O
The date of procedy completely for the process of t	Santa Clara, California 95054 fax (408) 727 564		OF 1



Harring Town Trans. 1000 **₹** of t σ<u>ζ</u> Maring, Browning 7. 788688410 receptace. Day SOAW weerst) -1 10642901 Night 5.27



10/5/51

# **Individual Tower Method-of-Moments Modeling Data**

#### Tower 1

C:\Expert MININEC Broadcast Professional\Files\KLOK\_TWR1 07-17-2009 07:34:05

KLOK Tower 1

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.29	12
		0	0	100.		
2	none	110.	70.	0	.44	12
		110.	70.	100.		
3	none	220.	70.	0	.29	12
		220.	70.	99.		

Number of wires = 3 current nodes = 36

minimum		max	imum	
Individual wires	wire	value	wire	value
segment length	3	8.25	1	8.33333
radius	1	.29	2	.44

#### ELECTRICAL DESCRIPTION

Frequencies (MHz)

	trequency		no. of	segment length	(wavelengths)
no.	lowest	step	steps	minimum	maximum
1	1.17	0	1	.0229167	.0231481

#### Sources

source	node	sector	magnitude	phase	type
1	1	1	1.	Ō	current

#### Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	13	0	-10,000.	0	0	0
2	25	0	-10,000.	0	0	0
3	1	0	0	.0037	0	0

Resistivity (ohm-meter) = 0.0000002

C:\Expert MININEC Broadcast Professional\Files\KLOK\_TWR1 08-07-2009 07:51:23

#### IMPEDANCE

normalization = 50.

freq	resist	react	imped	phase	VSWR	S11	S12
(MHz)	(ohms)	(ohms)	(ohms)	(deg)		dB	dB
source =	1; node	1, secto	or 1				
1.17	59.807	100.59	117.02	59.3	5.2242	-3.3668	-2.6809



# Individual Tower Method-of-Moments Modeling Data

C:\Expert MININEC Broadcast Professional\Files\KLOK\_TWR1 08-07-2009 07:51:23 CURRENT rms Frequency = 1.17 MHzInput power = 29.9035 watts Efficiency = 99.94 % coordinates in degrees current mag phase real imaginary no. Υ (amps) (deg) (amps) (amps) GND 0 0 0 .707107 0 .707107 2 0 0 8.33333 .745705 357.3 .744859 -.0355033 3 0 0 16.6667 .755852 355.7 .753712 -.0568355 4 0 0 25. .747451 354.5 .743961 -.0721419 5 0 0 33.3333 .721914 353.5 .717204 -.0823291 6 0 0 41.6667 .680224 352.6 .674542 -.0877329 7 0 0 50. .623325 351.8 .617006 -.0885298 8 0 0 58.3333 .552275 351.2 .545716 -.0848648 9 0 0 66.6667 .468211 350.5 .461855 -.0768837 10 0 75. 0 .372233 350. .366561 -.0647342 11 0 0 83.3333 .265093 349.5 .260618 -.0485027 12 0 0 91.6667 .146261 349. .14355 -.028026 END 100. 0 0 0 0 GND 37.6222 -103.366 0 2.65E-03 207.4 -2.35E-03 -1.22E-03 -103.366 8.33333 .0288868 207.4 -.0256463 -.0132935 -103.366 16.6667 .0435685 207.4 -.0386821 -.0200478 -103.366 25. .0538888 207.4 -.0478465 -.0247935 14 37.6222 15 37.6222 16 37.6222 .0538888 207.4 -.0478465 -.0247935 -103.366 25. -103.366 33.3333 17 37.6222 .0605327 207.4 -.0537478 -.0278459 -103.366 41.6667 .0637926 207.4 -.0566452 -.0293396 18 37.6222 19 37.6222 -103.366 50. .0638332 207.4 -.0566851 -.0293509 37.6222 -103.366 50. 37.6222 -103.366 58.3333 37.6222 -103.366 66.6667 20 .0607913 207.4 -.0539888 -.0279426 21 .0548021 207.4 -.0486759 -.025178 37.6222 -103.366 75. 22 .0459947 207.3 -.0408602 -.0211178 37.6222 -103.366 83.3333 23 .0344466 207.3 -.0306086 -.0158014 24 37.6222 -103.366 91.6667 .0200585 207.3 -.0178296 -9.19E-03 37.6222 -103.366 100. END 0 0 0 0 GND 75.2444 -206.732 0 1.79E-03 101.5 

 -206.732
 0
 1.79E-03
 101.5
 -3.56E-04
 1.75E-03

 -206.732
 8.25
 .0166976
 101.4
 -3.3E-03
 .016368

 -206.732
 16.5
 .0256207
 101.3
 -5.02E-03
 .0251243

 -206.732
 24.75
 .0319967
 101.2
 -6.2E-03
 .0313905

 -206.732
 33.
 .036207
 101.
 -6.92E-03
 .0355387

 -206.732
 41.25
 .0383925
 100.9
 -7.24E-03
 .0377043

 -206.732
 49.5
 .0386249
 100.7
 -7.16E-03
 .0379546

 -206.732
 57.75
 .0369604
 100.5
 -6.73E-03
 .0363416

 -206.732
 66.
 .0334553
 100.3
 -5.98E-03
 .0329168

 -206.732
 74.25
 .0281633
 100.1
 -4.93E-03
 .0277293

 -3.56E-04 1.75E-03 26 75.2444 27 75.2444 28 75.2444 29 75.2444 30 75.2444 31 75.2444 32 75.2444 33 75.2444 34 75.2444 -206.732 74.25 .0281633 100.1 -4.93E-03 .0277293 35 75.2444 -206.732 82.5 .0211106 99.8 -3.61E-03 .0208005 36 75.2444 -206.732 90.75 .0122116 99.6 -2.03E-03 .0120416 END 75.2444 -206.732 99. 0 0



# Individual Tower Method-of-Moments Modeling Data

#### Tower 2

C:\Expert MININEC Broadcast Professional\Files\KLOK\_TWR2 07-17-2009 07:37:17

KLOK Tower 2

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire	caps	Distance	Angle	$\mathbf{z}$	radius	segs
1	none	0	0	0	.29	12
		0	0	100.		
2	none	110.	70.	0	.44	12
		110.	70.	100.		
3	none	220.	70.	0	.29	12
		220.	70.	99.		

Number of wires current nodes = 36

	max	imum		
Individual wires	wire	value	wire	value
segment length	3	8.25	1	8.33333
radius	1	.29	2	.44

#### ELECTRICAL DESCRIPTION

Frequencies (MHz)

	frequency		no. of	segment leng	th (wavelengths)
no.	lowest	step	steps	minimum	maximum
1	1.17	0	1	.0229167	.0231481

#### Sources

source	node	sector	magnitude	phase	type
1	13	1	1.	0	current

### Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	13	0	0	.0034	ò	0
2	25	0	-10,000.	0	0	0
3	1	0	-10,000.	0	0	0

Resistivity (ohm-meter) = 0.0000002

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#### IMPEDANCE

normalization = 50.

freq	resist	react	imped	phase	VSWR	S11	S12
	(ohms)		_	(deg)		dB	dB
source =	1; node	13, sect	or 1				
1.17	59.043	96.063	112.76	58.4	4.9516	-3.5572	-2.5246



# Individual Tower Method-of-Moments Modeling Data

curre	arnaces in	degrees				_	
no.	X	Y	Z	mag	phase	real	imaginary
GND	0	0	0	(amps)	(deg)	(amps)	(amps)
2	0	0	8.33333	2.65E-03			-1.22E-03
3	0	0		.024834	207.4	0220491	
4	0	0	16.6667	.0380523			0175072
5	0	0	25.	.0474131			0218122
6	0	0	33.3333 41.6667	.0534975			0246094
7	0	0		.0565361		0502003	
8	0	0	50.	.0566625			0260606
9	0	0	58.3333	.0539934			0248297
10	0	0	66.6667	.0486497		0432027	
11	0	0	75.	.0407522			0187307
12	0	0	83.3333	.0303844			0139584
END	0	0	91.6667	.017473	207.3		-8.02E-03
GND	37.6222	-	100.	0	0	0	0
14	37.6222	-103.366	0	.707107	0	.707107	0
15	37.6222	-103.366	8.33333	.752394	356.8	.751251	0414548
16	37.6222	-103.366	16.6667	.764986	355.1	.762233	0648432
17	37.6222	-103.366	25.	.758387	353.8	.753995	0814969
18	37.6222	-103.366	33.3333	.734132	352.8	.728285	0924712
19	37.6222	-103.366	41.6667	.693272	351.9	.686283	0981931
20	37.6222	-103.366	50.	.636774	351.1	.629049	0988825
21	37.6222	-103.366	58.3333	.565688	350.4	.557704	0947078
22	37.6222	-103.366	66.6667	.481126	349.7	.473408	08583
23	37.6222	-103.366 -103.366	75.	.384135	349.1	.37725	0724014
24	37.6222		83.3333	.275347	348.6	.269902	05449
END	37.6222	-103.366	91.6667	.154085	348.1	.15075	0318846
GND	75.2444	-103.366	100.	0	0	0	0
26	75.2444	-206.732	0	2.6E-03	207.7	-2.3E-03	-1.21E-03
27	75.2444	-206.732 -206.732	8.25	.0242034		0214246	
28	75.2444		16.5	.0370534		0327998	
29	75.2444	-206.732 -206.732	24.75	.0461486		0408515	
30	75.2444		33.	.0520589		0460838	
31	75.2444	-206.732	41.25	.0550108		0486975	
32	75.2444	-206.732	49.5	.0551354		0488085	
33	75.2444	-206.732	57.75	.0525455		0465168	
34	75.2444	-206.732	66.	.0473568		0419251	
34 35	75.2444	-206.732	74.25	.0396836		0351344	
35 36	75.2444 75.2444	-206.732	82.5	.0296027		0262122	
		-206.732	90.75	.0170367		0150882	
END	75.2444	-206.732	99.	0	0	0	0

# Individual Tower Method-of-Moments Modeling Data

#### Tower 3

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KLOK Tower 3

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	segs
1	none	0	0	0	.29	12
		0	0	100.		
2	none	110.	70.	0	.44	12
		110.	70.	100.		
3	none	220.	70.	0	.29	12
		220.	70.	99.		

Number of wires current nodes = 36

minimum			max	imum
Individual wires	wire	value	wire	value
segment length	3	8.25	1	8.33333
radius	1	.29	2	.44

#### ELECTRICAL DESCRIPTION

Frequencies (MHz)

	frequency		no. of	segment 1	ength (wavelengths)
no.	lowest	step	steps	minimum	maximum
1	1.17	0	1	.0229167	.0231481

#### Sources

source	node	sector	magnitude	phase	type
1	25	1	1.	Ō	current

#### Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	13	0	-10,000.	0	0	0
2	25	0	0	.0028	0	0
3	1	0	-10,000.	0	0	0

Resistivity (ohm-meter) = 0.0000002

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#### IMPEDANCE

normalization = 50.

freq	resist	react	imped	phase	VSWR	S11	S12
(MHz)	(ohms)	(ohms)	(ohms)	(deg)		dB	dB
source =	1; node	25, sect	or 1				
1.17	57.511	88.368	105.43	56.9	4.5137	-3.9136	-2.2629



### Individual Tower Method-of-Moments Modeling Data

C:\Expert MININEC Broadcast Professional\Files\KLOK\_TWR3 08-07-2009 CURRENT rms Frequency = 1.17 MHzInput power = 28.7556 watts Efficiency = 99.94 % coordinates in degrees current mag phase real imaginary no. Х 7. (amps) (deg) (amps) (amps) GND Λ 0 1.79E-03 101.5 -3.55E-04 1.75E-03 0 2 0 8.33333 .0168049 101.4 -3.32E-03 .0164741 3 0 16.6667 .0258088 101.3 -5.05E-03 .0253102 0 4 0 0 .0322464 101.2 -6.24E-03 .0316376 25. 5 0 0 33.3333 .0364993 101. -6.97E-03 .0358281 6 0 0 41.6667 .0387073 100.8 -7.28E-03 .0380164 7 Λ 0 .038942 100.7 -7.21E-03 .0382694 50. 8 0 0 58.3333 .0372599 100.5 -6.77E-03 .0366394 9 Ω 0 66.6667 .0337193 100.3 -6.01E-03 .0331798 10 n 0 75. .0283762 100. -4.95E-03 .0279417 11 0 0 83.3333 .02126 99.8 -3.62E-03 .02095 12 0 91.6667 0 .0122889 99.5 -2.03E-03 .0121192 100. END 0 0 0 0 0 37.6222 -103.366 0 37.6222 -103.366 8.3 GND 2.6E-03 207.7 -2.3E-03 -1.21E-03 -103.366 8.33333 .0283321 207.7 -.0250811 -.0131775 -103.366 16.6667 .0427291 207.7 -.0378261 -.0198737 -103.366 25. .0528464 207.7 -.0467825 -.0245794 -103.366 33.3333 .0593566 207.7 -.0525458 -.0276069 -103.366 41.6667 .0625472 207.7 -.055371 -.0290896 14 37.6222 15 16 37.6222 17 37.6222 18 37.6222 -103.366 50. 19 37.6222 .0625809 207.7 -.0554023 -.0291025 -103.366 50. -103.366 58.3333 20 37.6222 .0595927 207.7 -.0527595 -.0277078 37.6222 -103.366 21 66.6667 .0537163 207.7 -.047561 -.0249678 22 37.6222 -103.366 75. .045079 207.7 -.0399189 -.0209427 23 37.6222 -103.366 83.3333 -.0298996 -.0156713 .0337576 207.7 37.6222 24 -103.366 91.6667 .0196554 207.6 -.0174144 -9.11E-03 END 37.6222 -103.366 100. 0 0 0 GND 75.2444 -206.732 0 .707107 0 .707107 26 75.2444 -206.732 8.25 .742078 357.4 .741302 -.0339181 75.2444 27 -206.732 16.5 .749999 355.9 .748034 -.0542596 75.2444 -206.732 24.75 28 .740029 354.7 .736819 -.0688469 29 75.2444 -206.732 33. .713509 353.7 .709172 -.0785518 30 75.2444 -206.732 41.25 .671363 352.8 .666125 -.0837002 75.2444 31 -206.732 49.5 .614519 352.1 .608687 -.0844625 32 75.2444 -206.732 57.75 .543995 351.4 .537935 -.080975 33 75.2444 -206.732 66. .460886 350.8 .455008 -.0733772 34 75.2444 -206.732 74.25 .366242 350.3 .36099 -.0618029

.260763 349.8

.143882 349.3 .141366

.256614

-.0463291

-.0267905



75.2444

75.2444

75.2444

-206.732 82.5

-206.732 90.75

-206.732 99.

35

36

END

07:55:36

# **Expert MININEC Broadcast Professional Daytime Method-of-Moments Modeling Data**

C:\Expert MININEC Broadcast Professional\Files\KLOK\_D 08-07-2009 08:48:47

MEDIUM WAVE ARRAY SYNTHESIS FROM FIELD RATIOS

Frequency = 1.17 MHz

#### field ratio tower magnitude phase (deg) 1 1. 02 1. 155. -145. 1.3 3

#### VOLTAGES AND CURRENTS - rms

source	voltage		current	
node	magnitude	phase (deg)	magnitude	phase (deq)
1	2,367.49	71.5	12.564	8.2
13	1,902.7	217.7	13.3742	165.
25	1,707.93	267.3	19.8922	221.9
Sum of	square of so	urce currents	= 1,464.85	
Total p	power = 52,65	0. watts		

#### TOWER ADMITTANCE MATRIX

admittance	real (mhos)	imaginary (mhos)
Y(1, 1)	.00471129	006683
Y(1, 2)	.00299077	9.0492E-05
Y(1, 3)	.000147503	00099249
Y(2, 1)	.00299078	9.0535E-05
Y(2, 2)	.0055954	00574914
Y(2, 3)	.00319596	.000243985
Y(3, 1)	.000147505	000992485
Y(3, 2)	.00319595	.000243975
Y(3, 3)	.00549868	0071265

#### TOWER IMPEDANCE MATRIX

impedance	real (ohms)	imaginary (ohms)
Z(1, 1)	59.8956	100.564
Z(1, 2)	17.2365	-32.9643
Z(1, 3)	-24.4781	-5.21652
Z(2, 1)	17.2359	-32.9644
Z(2, 2)	59.2677	95.9074
Z(2, 3)	17.0806	-32.2408
Z(3, 1)	-24.4781	-5.21636
Z(3, 2)	17.0807	-32.2408
Z(3, 3)	57.5965	88.3503



# Expert MININEC Broadcast Professional Daytime Method-of-Moments Modeling Data

C:\Expert MININEC Broadcast Professional\Files\KLOK\_D 08-07-2009 08:54:53 KLOK Day

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire 1	caps none	Distance 0	Angle 0	Z 0	radius .29	segs
		0	0	100.	123	12
2	none	110.	70.	0	.44	12
		110.	70.	100.		
3	none	220.	70.	0	.29	12
		220.	70.	99		**

Number of wires = 3 current nodes = 36

	mini	mum	maximum	
Individual wires	wire	value	wire	value
segment length	3	8.25	1	8.33333
radius	1	.29	2	.44

#### ELECTRICAL DESCRIPTION

Frequencies (MHz)

frequency no. lowest step 1 1.17 0	no. of	segment length	(wavelengths)
	steps	minimum	maximum
	1	.0229167	.0231481

#### Sources

sourc	e node	sector	magnitude	phase	type
1	1	1	3,348.13	71.5	voltage
2	13	1	2,690.82	217.7	voltage
3	25	1	2,415.38	267.3	voltage

#### Lumped loads

load 1 2	node 13 25	resistance (ohms) 0	reactance (ohms) 0	inductance (mH) .0034 .0028	capacitance (uF)	passive circuit 0
_		-	0	.0028	0	0
3	1	0	0	.0037	0	0

Resistivity (ohm-meter) = 0.0000002

C:\Expert MININEC Broadcast Professional\Files\KLOK\_D 08-07-2009 08:54:53

#### IMPEDANCE

normalization = 50.

freq (MHz)	resist (ohms)		phase (deg)	VSWR	S11 dB	S12 dB
source = 1.17			63.5	9.1024	-1.9162	••••



# Expert MININEC Broadcast Professional Daytime Method-of-Moments Modeling Data

```
source = 2; node 13, sector 1
          88.012
                   116.06
                           145.65
                                    52.8
                                             5.1966 -3.3851
                                                              -2.6653
 source = 3; node 25, sector 1
 1.17
          61.874
                   62.677
                            88.073
                                    45.4
                                             2.9798 -6.0648 -1.2347
 C:\Expert MININEC Broadcast Professional\Files\KLOK_D
                                                         08-07-2009
                                                                      08:54:53
CURRENT rms
Frequency
           = 1.17 \text{ MHz}
 Input power = 52,650. watts
Efficiency = 99.95 %
coordinates in degrees
current
                                     mag
                                              phase
                                                    real
                                                               imaginary
no.
       Х
                 Y
                           7.
                                              (deg)
                                     (amps)
                                                     (amps)
                                                               (amps)
GND
       0
                 0
                           Ω
                                     12.5969
                                              8.1
                                                     12.4715
                                                               1.77306
 2
       0
                 0
                           8.33333
                                     13.9693 4.5
                                                     13.9258
                                                               1.10243
 3
       0
                 0
                           16.6667
                                     14.6001 2.6
                                                     14.5855
                                                               .652672
 4
       0
                           25.
                 0
                                     14.7743 1.1
                                                     14.7715
                                                               .288428
 5
       0
                 0
                           33.3333
                                     14.5372 360.
                                                     14.5372
                                                               -6.97E-03
 6
       0
                 0
                                     13.9121
                           41.6667
                                              359.
                                                     13.9101
                                                               -.237826
 7
                                     12.9196
       0
                 0
                           50.
                                             358.2 12.9133
                                                               -.404892
 8
       0
                 0
                           58.3333
                                     11.5817
                                              357.5
                                                    11.5705
                                                               -.507921
 9
       0
                 0
                           66.6667
                                     9.92159
                                              356.8 9.90653
                                                               -.546518
 10
       0
                 0
                           75.
                                     7.96252
                                              356.3
                                                     7.9455
                                                               -.520306
 11
       Λ
                 0
                           83.3333
                                     5.72007
                                              355.7
                                                     5.704
                                                               -.428395
 12
       0
                 0
                           91.6667
                                     3.18184
                                              355.2
                                                    3.17059
                                                               -.267315
END
       0
                 0
                           100.
                                     0
                                              0
GND
       37.6222
                -103.366 0
                                     13.4094
                                              164.9
                                                     -12.9446
                                                               3.50003
                -103.366 8.33333
 14
       37.6222
                                     14.4611
                                              160.5
                                                     -13.632
                                                               4.8261
 15
       37.6222
                -103.366
                          16.6667
                                     14.8651
                                              158.1
                                                     -13.7936
                                                               5.54157
 16
       37.6222
                -103.366
                           25.
                                     14.863
                                              156.3
                                                     -13.6124
                                                               5.96763
 17
       37.6222
                -103.366
                           33.3333
                                     14.491
                                              154.9
                                                     -13.1222
                                                               6.14788
 18
       37.6222
                          41.6667
                -103.366
                                     13.7693 153.7
                                                     -12.3441
                                                               6.10059
 19
       37.6222
                -103.366
                          50.
                                     12.7163 152.7
                                                     -11.2973
                                                               5.83757
 20
       37.6222
                -103.366
                          58.3333
                                     11.352
                                              151.8
                                                    -10.0018
                                                               5.36951
 21
       37.6222
                -103.366
                          66.6667
                                     9.69789 151.
                                                     -8.47893
                                                               4.7071
 22
       37.6222
                -103.366
                          75.
                                     7.77439
                                             150.2
                                                     -6.74823
                                                               3.86038
 2.3
       37.6222
                -103.366
                          83.3333
                                     5.59379
                                             149.5
                                                     -4.82213
                                                               2.83506
 24
       37.6222
                -103.366
                          91.6667
                                     3.14161 148.9
                                                    -2.69005 1.62276
END
       37.6222 -103.366 100.
                                              0
                                                     0
                                                               0
GND
       75.2444
                -206.732 0
                                     19.9063 221.9
                                                    -14.8194 -13.2907
 26
       75.2444
                -206.732 8.25
                                     20.4155 219.1 -15.834
                                                               -12.8872
 27
       75.2444
                -206.732 16.5
                                     20.3743 217.4 -16.1781 -12.3848
 28
       75.2444
                -206.732 24.75
                                     19.9058 216.1
                                                    -16.0878
                                                              -11.7227
 29
       75.2444
                -206.732 33.
                                     19.0368 214.9
                                                    -15.6057
                                                              -10.9024
 30
       75.2444
                -206.732 41.25
                                     17.7887 213.9 -14.7569 -9.93339
 31
       75.2444
                -206.732
                          49.5
                                    16.1845 213.1
                                                    -13.564
                                                              -8.8293
 32
       75.2444
                -206.732 57.75
                                    14.2505 212.3
                                                    -12.0507 -7.60639
 33
       75.2444
                -206.732 66.
                                    12.015
                                             211.5 -10.242
                                                              -6.28186
       75.2444
 34
                -206.732
                          74.25
                                    9.50539 210.8 -8.16181
                                                             -4.8721
 35
       75.2444
                -206.732
                          82.5
                                    6.73985 210.2 -5.82602
                                                              -3.38866
 36
       75.2444
                -206.732
                          90.75
                                    3.70424 209.6 -3.22225 -1.82717
END
       75.2444
                -206.732
                          99.
                                             0
                                                     0
```



# Expert MININEC Broadcast Professional Nighttime Method-of-Moments Modeling Data

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MEDIUM WAVE ARRAY SYNTHESIS FROM FIELD RATIOS

Frequency = 1.17 MHz

# field ratio tower magnitude phase (deg) 1 1. -93. 2 1.92 0 3 1. 93.

#### VOLTAGES AND CURRENTS - rms

source	voltage		current	
node	magnitude	phase (deg)	magnitude	phase (deg)
1	712.445	322.5	3.43068	283.
13	807.508	64.2	7.07749	7.6
25	272.164	166.4	4.04173	95.7
Sum of	square of so	urce currents	= 156.392	
Total p	power = 5,400	. watts		

#### TOWER ADMITTANCE MATRIX

admittance	real (mhos)	imaginary (mhos)
Y(1, 1)	.00471129	006683
Y(1, 2)	.00299077	9.0492E-05
Y(1, 3)	.000147503	00099249
Y(2, 1)	.00299078	9.0535E-05
Y(2, 2)	.0055954	00574914
Y(2, 3)	.00319596	.000243985
Y(3, 1)	.000147505	000992485
Y(3, 2)	.00319595	.000243975
Y(3, 3)	.00549868	0071265

#### TOWER IMPEDANCE MATRIX

ımpedance	real (ohms)	imaginary	(ohms)
Z(1, 1)	59.8956	100.564	, ,
Z(1, 2)	17.2365	-32.9643	
Z(1, 3)	-24.4781	-5.21652	
Z(2, 1)	17.2359	-32.9644	
Z(2, 2)	59.2677	95.9074	
Z(2, 3)	17.0806	-32.2408	
Z(3, 1)	-24.4781	-5.21636	
Z(3, 2)	17.0807	-32.2408	
Z(3, 3)	57.5965	88.3503	

### **Expert MININEC Broadcast Professional** Nighttime Method-of-Moments Modeling Data

C:\Expert MININEC Broadcast Professional\Files\KLOK\_N 08-07-2009 09:37:22 KLOK Night

#### GEOMETRY

Wire coordinates in degrees; other dimensions in meters Environment: perfect ground

wire	caps	Distance	Angle	Z	radius	seqs
1	none	0	0	0	.29	12
		0	0	100.		
2	none	110.	70.	0	.44	12
		110.	70.	100.		
3	none	220.	70.	0	.29	12
		220.	70.	99.		

Number of wires current nodes = 36

	mini	mum	maximum	
Individual wires	wire	value	wire	value
segment length	3	8.25	1	8.33333
radius	1	.29	2	.44

#### ELECTRICAL DESCRIPTION

Frequencies (MHz)

	frequency		no. of	segment length	(wavelengths)
no.	lowest	step	steps	minimum	maximum
1	1.17	0	1	.0229167	.0231481

#### Sources

source	node	sector	magnitude	phase	type
1	1	1	1,007.55	322.5	voltage
2	13	1	1,141.99	64.2	voltage
3	25	1	384.899	166.4	voltage

#### Lumped loads

load	node	resistance (ohms)	reactance (ohms)	inductance (mH)	capacitance (uF)	passive circuit
1	13	0	0	.0034	0	0
2	25	0	0	.0028	0	0
3	1	0	0	.0037	0	0

Resistivity (ohm-meter) = 0.0000002

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#### IMPEDANCE

normalization = 50.

freq	resist	react	imped	phase	VSWR	S11	S12
(MHz)	(ohms)	(ohms)	(ohms)	(deg)		dB	dB
source =	1; node	1, secto	or 1				
1.17	159.67	132.21	207.3	39.6	5.5147	-3.1853	-2.8421



### Expert MININEC Broadcast Professional Nighttime Method-of-Moments Modeling Data

```
source = 2; node 13, sector 1
 1.17
          62.583
                   95.148
                             113.88
                                      56.7
                                               4.7325 -3.7269
                                                                -2.3954
 source = 3; node 25, sector 1
 1.17
          22.225
                   63.544
                             67.319
                                      70.7
                                               6.1655 -2.8427 -3.1847
 C:\Expert MININEC Broadcast Professional\Files\KLOK N
                                                            08-07-2009
                                                                         09:37:22
 CURRENT rms
            = 1.17 MHz
 Frequency
 Input power = 5,400. watts
 Efficiency = 99.96 %
 coordinates in degrees
 current
                                       maq
                                                phase
                                                      real
                                                                  imaginary
 no.
        Х
                            \mathbf{z}
                                       (amps)
                                                (deq)
                                                       (amps)
                                                                  (amps)
 GND
        0
                  0
                            0
                                       3.43812
                                                282.8
                                                       .76459
                                                                  -3.35202
 2
        0
                  0
                            8.33333
                                       3.73112
                                                275.9
                                                       .384983
                                                                 -3.71121
 3
        0
                  0
                            16.6667
                                       3.87118
                                                272.
                                                       .136171
                                                                  -3.86878
  4
        0
                  0
                            25.
                                       3.9049
                                                269.1 -.0591137 -3.90445
 5
        0
                  0
                            33.3333
                                       3.8375
                                                266.9 -.210806 -3.83171
  6
        0
                  0
                            41.6667
                                       3.67185
                                               265.
                                                       -.321928
                                                                 -3.65771
 7
        0
                  0
                            50.
                                       3.41135
                                               263.4
                                                      -.393604
                                                                 -3.38856
 8
        0
                  0
                            58.3333
                                       3.06041
                                                262.
                                                       -.426482
                                                                 -3.03054
 9
        0
                  0
                            66.6667
                                               260.8
                                       2.62429
                                                      -.421193
                                                                 -2.59027
 10
                  0
                            75.
                                       2.10841
                                               259.7
                                                       -.378396
                                                                 -2.07417
 11
                  0
                            83.3333
                                       1.51636
                                                258.7
                                                       -.298412
                                                                 -1.48671
 12
       0
                  0
                            91.6667
                                      .84449
                                                257.7
                                                      -.179893
                                                                 -.825107
END
                            100.
                                      0
                                                0
                                                       0
GND
       37.6222
                 -103.366 0
                                      7.09348
                                               7.5
                                                       7.03238
                                                                 .929024
 14
       37.6222
                 -103.366
                           8.33333
                                      7.51786
                                               4.3
                                                       7.49685
                                                                 .561721
 15
       37.6222
                 -103.366
                           16.6667
                                      7.64556
                                               2.5
                                                       7.63854
                                                                 .327573
 16
       37.6222
                 -103.366
                           25.
                                      7.57971
                                               1.1
                                                       7.57841
                                                                 .14048
 17
       37.6222
                 -103.366
                           33.3333
                                      7.33769
                                               359.9
                                                       7.33768
                                                                 -9.61E-03
 18
       37.6222
                 -103.366
                           41.6667
                                      6.92976
                                               359.
                                                       6.92862
                                                                 -.125755
 19
       37.6222
                 -103.366
                           50.
                                      6.36556
                                               358.1
                                                       6.36213
                                                                 -.208894
 20
       37.6222
                           58.3333
                 -103.366
                                      5.65549
                                               357.4
                                                       5.64954
                                                                 -.259371
 21
       37.6222
                 -103.366
                           66.6667
                                      4.81056
                                               356.7
                                                       4.80255
                                                                 -.2774
 22
       37.6222
                 -103.366
                           75.
                                      3.84119
                                               356.1
                                                       3.83217
                                                                 -.263167
 23
       37.6222
                 -103.366
                           83.3333
                                      2.75366
                                               355.5
                                                       2.74513
                                                                 -.21655
 24
       37.6222
                 -103.366 91.6667
                                      1.54112 354.9 1.53509
                                                                 -.13617
END
       37.6222
                 -103.366 100.
                                      0
                                               0
                                                       0
                                                                 n
GND
       75.2444
                 -206.732 0
                                      4.04456 95.6
                                                      -.39744
                                                                 4.02499
 26
       75.2444
                 -206.732
                           8.25
                                      4.15209 94.6
                                                      -.334803
                                                                4.13857
 27
       75.2444
                 -206.732
                           16.5
                                      4.14219 94.
                                                      -.287962
                                                                 4.13217
 28
       75.2444
                 -206.732 24.75
                                      4.04365
                                              93.5
                                                      -.244734
                                                                 4.03624
 29
       75.2444
                 -206.732
                           33.
                                      3.86318 93.
                                                      -.203867
                                                                3.85779
 30
       75.2444
                 -206.732
                           41.25
                                      3.60581 92.6
                                                      -.165316
                                                                3.60201
 31
       75.2444
                 -206.732
                           49.5
                                      3.27672 92.3
                                                      -.129443
                                                                3.27416
 32
       75.2444
                 -206.732
                           57.75
                                      2.88164 91.9
                                                      -.0967641 2.88002
 33
       75.2444
                 -206.732
                           66.
                                     2.42661 91.6
                                                      -.0678464 2.42566
 34
       75.2444
                 -206.732
                           74.25
                                      1.9174
                                               91.3
                                                      -.0432497 1.91691
 35
       75.2444
                 -206.732
                           82.5
                                     1.35788 91.
                                                      -.0234868 1.35768
 36
       75.2444
                 -206.732
                           90.75
                                      .745375 90.7
                                                      -9.E-03
                                                                .74532
END
       75.2444
                 -206.732
                           99.
                                               0
                                                      0
```



### **Sample System Proof**

# Sample Line Length

Tower	Sample Line 3/4λ Resonance	Sample Line 5/4λ Resonance	Sample Line Length at 1210 kHz	Measured Impedance at at 1210 kHz with Toroid
1	1016.9 kHz	1694.8 kHz	310.7°	49.57 - j2.06 Ω
2	1016.9	1694.8	310.7°	49.48 - i2.13
3	1016.9	1694.8	310.7°	49.47 - i2.00

# Sample Line Characteristic Impedance

Tower	-45° Offset Frequency	-45° Measured Impedance	+45° Offset Frequency	+45° Offset Impedance	Calculated Characteristic Impedance
1	947 4 LTI-				
1	847.4 kHz	$5.37 - j49.90 \Omega$	1186.4 kHz	$8.04 + j49.68 \Omega$	$50.3~\Omega$
2	847.4	5.39 – j50.16	1186.4	8.08 + j49.65	50.4
3	847.4	5.39 - j50.57	1186.4	8.07 + j49.83	50.7

Based upon the characteristic impedance formula:  $Z = ((R12 + X12)^{1/2} * (R22 + X22)^{1/2})^{1/2}$ 



# **Reference Point Measurements**

# Daytime Radial 16.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
2.45 km	760.0	37° 19' 57.4" N 121° 48' 30.4" W	NE corner of Glen Hanleigh & Glen Dundee
3.59 km	580.0	37° 20' 32.8" N 121° 48' 18.3" W	In front of 319 Flinthaven Dr.
4.58 km	330.0	37° 21' 03.7" N 121° 48' 08.3" W	In front of 3402 Rocky Mountain Dr.

# Daytime Radial 70.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
2.20 km	670.0	37° 19' 06.7" N 121° 47' 34.0" W	In front of 2719 White Acres Dr.
3.00 km	520.0	37° 19' 14.4" N 121° 47' 04.0" W	In front of 3127 Mt Isabel Ct.
4.05 km	360.0	37° 19' 31.7" N 121° 46' 08.9" W	E. side of driveway for 3555 Coeur de Charles

# Daytime Radial 160.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
3.00 km	370.0	37° 17' 09.7" N 121° 48' 16.3" W	0.14 mi E. on Hassler Pkwy from Dove Hill Rd.
4.25 km	198.0	37° 16' 32.4" N 121° 47' 59.4" W	On Coyote Rd., 100' west of Scarlett Ave.
5.40 km	164.0	37° 15' 56.1" N 121° 47' 42.3" W	At the intersection of Coyote Rd. and Tigerwood

# Daytime Radial 340.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
2.18 km	600.0	37° 19' 45.6" N 121° 49' 29.2" W	SW corner of Ceylon Ave. and Ceylon Ct.
3.35 km	333.0	37° 20' 23.0" N 121° 49' 45.5" W	In front of 2154 Simon Ave.
4.77 km	250.0	37° 21' 05.5" N 121° 50' 05.3" W	NE corner of Bambi Ln. and Cottentail Ln.



# **Reference Point Measurements**

# Nighttime Radial 20.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
2.30 km	72.0	37° 19' 51.1" N 121° 48' 25.7" W	In front of 2462 Glen Duff Way
3.30 km	36.0	37° 20' 21.5" N 121° 48' 11.4" W	In E. entrance for Lake Cunningham Pk. @ S. White Rd.
4.58 km	28.0	37° 21' 00.8" N 121° 47' 55.0" W	In front of 3469 Mt Prieta Dr.

# Nighttime Radial 50.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
2.00 km	10.5	37° 19' 23.4" N 121° 47' 55.6" W	Opp. 2866 Burdick Way
3.15 km	12.0	37° 19' 47.1" N 121° 47' 20.2" W	In front of 3308 Remington Way
4.05 km	7.4	37° 20' 05.6" N 121° 46' 51.6" W	In front of 3449 Cedardale Dr.

# Nighttime Radial 70.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
2.20 km	20.0	37° 19' 06.7" N 121° 47' 34.0" W	In front of 2719 White Acres Dr.
3.00 km	15.1	37° 19' 14.4" N 121° 47' 04.0" W	In front of 3127 Mt Isabel Ct.
4.05 km	11.0	37° 19' 31.7" N 121° 46' 08.9" W	E. side of driveway for 3555 Coeur de Charles.

### Nighttime Radial 110.0°T

Distance	Field (mV/m)	Coordinates (NAD27)	Description
2.00 km	16.50	37° 18' 18.9" N 121° 47' 42.3" W	SW corner of Ceylon Ave. and Ceylon Ct
3.50 km	5.0	37° 18' 02.4" N 121° 46' 44.7" W	In front of 2154 Simon Ave.
4.65 km	6.2	37° 17' 50.8" N 121° 46' 00.5" W	NE corner of Bambi Ln. and Cottentail Ln.



# **Harmonic and Spurious Measurements**

Frequency	dB below 1170 Carrier
750 kHz <sup>†</sup>	< -80
910 <sup>*</sup>	(KNEW)
2340	-86.4
2600*	< -110
2760†	< -110
3510	-109.9
3770 <sup>*</sup>	< -110
3930 <sup>†</sup>	< -110

Measurements made 1 km from station.

<sup>†</sup> Possible intermodulation product with KVVN, 1430 kHz, located 4.9 km from KLOK.



Possible intermodulation product with KLIV, 1590 kHz, located 4.9 km from KLOK. The adjacent channel signal of Radio Station KCBS was in the minima of the receiving antenna at the selected measurement location.